# Optimization of Low Stress PECVD Silicon Nitride

for GaAs Manufacturing



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Unaxis solutions for plasma-enhanced chemical vapor deposition (PECVD) silicon nitride (SiN<sub>x</sub>) are used extensively in the production of GaAs devices. PECVD is compatible with the low temperature constraints required for GaAs device manufacturing. With this technique, high quality SiN<sub>x</sub> can be deposited at temperatures less than 400°C. PECVD SiN<sub>x</sub> is used in many different GaAs-based devices such as MESFETs, HBTs, and HEMTs. In these devices, PECVD SiN<sub>x</sub> is typically used for passivation, encapsulation, and as a capping layer. In addition, the large dielectric constant of SiN<sub>x</sub> makes it attractive for use as the intermetallic dielectric in MIM capacitors.

It is well recognized that the stress of the SiN<sub>x</sub> layer in GaAs-based device structures can impact the electrical performance and lead to degradation. For GaAs MESFET and HEMT devices, it has been demonstrated not only the magnitude of the stress but also the stress state, compressive or tensile, can affect the performance [1]. Stressinduced failure via microvoid formation in SiN<sub>x</sub> MIM capacitors has also been reported [2]. Therefore, the capability of tailoring the magnitude and state of the SiN<sub>x</sub> stress required for a specific device structure is very important.

For SiN<sub>x</sub>, a common technique to control the stress in a conventional 13.56 MHz parallel plate PECVD reactor is through the addition of low frequency power. At 13.56 MHz, SiN<sub>x</sub> films prepared from standard gas mixtures of SiH<sub>4</sub>, NH<sub>3</sub>, and N<sub>2</sub> are typically tensile in nature. The added low frequency (< 1 MHz) component results in high energy ion bombardment of the growing SiN<sub>x</sub> film. This results in a change of the stress state from tensile to compressive [**3**, **4**]. At Unaxis, a He dilution method has been developed as a simpler alternative technique to control the stress of PECVD SiN<sub>x</sub>. As illustrated in *Figure 1*, the addition of He to the standard gas mixture of SiH<sub>4</sub>, NH<sub>3</sub>, and N<sub>2</sub>, enables stress control from about 300 MPa, tensile through zero to about –300 MPa, compressive.

Plasma-induced damage during the SiN<sub>x</sub> deposition process, resulting in physical and electronic degradation of GaAs devices is a very important issue [5–7]. Without the requirement of a low frequency power source, the possibility of damage is reduced with the He dilution

method. The RF power density at 13.56 MHz is very low and typically less than 50 mW/cm<sup>2</sup>.

A designed experiment (DOE) was implemented to characterize and optimize a low stress SiN<sub>x</sub> process based on the He dilution method on a Unaxis PECVD production platform developed for high volume GaAs manufacturing. To understand the mechanism involved in this technique for stress control, optical spectroscopic analysis of different He/N<sub>2</sub> plasmas in the PECVD reactor has been performed.

# Experimental

All the SiN<sub>x</sub> films were prepared on 100 mm Si test wafers from gas mixtures of SiH<sub>4</sub>, NH<sub>3</sub>, N<sub>2</sub>, and He on a Unaxis VERSALOCK<sup>®</sup> PECVD system [8]. This fully automated cassette-to-cassette

system is capable of batch handling eight 100 mm GaAs or five 150 mm GaAs wafers. The PECVD reactor is a conventional parallel plate configuration and uses a 13.56 MHz RF power source to generate the plasma. Wafer temperature can be controlled over a range of 100°C to 350°C. To obtain a high yield and minimize system downtime, several features in the PECVD reactor have been implemented to maintain system cleanliness. For example, both the chamber walls and the upper gas distribution electrode of the reactor are heated to minimize particulate formation during the SiN<sub>x</sub> deposition process. In addition, an automated plasma etchback sequencer interfaced to an in-situ optical emission spectrometer is used to achieve and consistently maintain the reactor in a clean state. Single wafer modules with either manual or automatic loading are also available for situations where batch processing is unnecessary.

For process optimization, a two level full factorial design on three factors was constructed for the DOE. The three factors were  $NH_3$  gas flow rate,  $N_2/(N_2+He)$  gas flow ratio, and RF power. All films were deposited at 300°C. The diluted SiH<sub>4</sub> gas flow rate, process pressure, and the combined  $N_2$  and He gas flow rates were held constant during the experiments.

The measured responses were refractive index, deposition rate, thickness non-uniformity, stress, and wet-etch rate. The thickness non-uniformity is defined as the thickness range divided by twice the mean thickness expressed as a percentage. The edge exclusion was 6 mm. A buffered oxide etch (BOE)



Figure 1: Stress control of PECVD Sin<sub>x</sub> by the He dilution method at the different rf power levels indicated

Responses							
		Index	Dep rate	Thickness non-uniformity	Stress	Etch rate	
Factors	↑ NH <sub>3</sub>	$\uparrow$ $\uparrow$	-	-	1	<b>↑ ↑</b>	
	<b>↑</b> % N <sub>2</sub> / He	Ŷ	1	$\downarrow \downarrow$	1	<b>↑ ↑</b>	
	↑ Power	Ť	<b>↑ ↑</b>	<b>↑ ↑</b>	Ŷ	$\uparrow$ $\uparrow$	

solution of 7:1  $NH_4F$  : HF was used for the wet-etch rate measurements.

### **Designed experiment results**

In *Figure 2*, the general response trends from the analyzed DOE are summarized. The up and down arrows indicate the directional change in the response resulting from an increase in a process factor, NH<sub>3</sub> gas flow rate, N<sub>2</sub> concentration in He, or RF power. Double and single arrows respectively indicate a strong or weak dependence of a response on a factor over the range investigated. All three factors have a major influence on the SiN<sub>x</sub> film stress. The measured film stresses ranged from about 300 MPa, tensile to about 400 MPa, compressive.

### Figure 2: General response trends from DOE

## Low stress optimization

Figure 3 summarizes the typical customer property requirements for a low stress SiN<sub>x</sub> film. Figure 4 maps out the predicted process space from the DOE for these criteria as a function of NH<sub>3</sub> gas flow rate and N<sub>2</sub>/He concentration in the plasma. These results clearly indicate a practical process regime exists to achieve a lowstress silicon nitride film to meet the desired criteria. The deposition rate for the low stress films is greater than 100 Å/min. Faster deposition rates are possible with either higher RF power or more concentrated SiH<sub>4</sub>.

### Stress control mechanism

Examination of the optical emission spectra of the deposition plasma provides important insight concerning the mechanism responsible for compressive stress by the He dilution method. Shown in Figure 5 are two 13.56 MHz plasma spectra, pure  $N_2$  and 10%  $N_2/He.$  These correspond to deposition conditions associated with tensile and compressive films. Emission lines at 391.4 nm and 427.8 nm are present in the 10% N<sub>2</sub>/He plasma and are absent in the pure N<sub>2</sub> plasma. These two lines are assigned to N<sub>2</sub><sup>+</sup> ions and indicate its presence in the 10% N<sub>2</sub>/He plasma. As shown in Figure 5, these N2<sup>+</sup> spectral lines are also present in a 380 kHz N<sub>2</sub> plasma without any He dilution. SiN<sub>x</sub> films prepared from SiH<sub>4</sub>,

Figure 3: Criteria for low-stress SiN<sub>x</sub> process optimization.

Film parameter	Range					
Stress (MPa)	-100 to +100					
Refractive index	2.0 to 2.05					
Thickness non-uniformity (%)	< ± 2.5					
Wet-etch rate (Å/min)	> 300					



Figure 4: Overlay plot for an optimized low stress SiN<sub>x</sub> process. Non-shaded area is the optimized process regime. Point in center denotes center point of the design.

Figure 5: Optical emission spectra for various plasmas. Spectra are displaced vertically for clarity.

